

# APPLICATION OF IEC 61853 MATRIX TO BIFACIAL PV

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**TNO** innovation  
for life



- › History:
  - › STC most important, and longest history in PV world.
  - › Additional parameters (e.g. NOCT) introduced in last couple of decades.

**Is it possible to calculate the full year yield based on these datasheet value ?**

- › **New** 61853 defines 7  $G_{POA}$  x 4  $T_{mod}$  matrix, leaving out the non-existing points:

Irradiance $W \cdot m^{-2}$	Spectrum	Module temperature			
		15 °C	25 °C	50 °C	75 °C
1 100	AM1,5	NA			
1 000	AM1,5		STC		
800	AM1,5				
600	AM1,5				
400	AM1,5				NA
200	AM1,5			NA	NA
100	AM1,5			NA	NA

# INTRODUCTION 'THE IEC-61853 MATRIX'

- › Objective of 61853: **Testing and rating** of a PV-module (under well-defined climatic conditions)
  - › Part 1: Irradiance and Temperature performance measurements and power rating
  - › Part 2: Spectral responsivity, incidence angle, and module operating temperature
  - › Part 3: Calculation of Energy Rating of PV modules
  - › Part 4: Standard Reference Climatic Profiles
  
- › Spectral-effects are described also in 61853:2, but less important than the matrix → Future work

- › Our contribution:
  - › additional visualization and statistics
  - › for the **Research Purpose** of understanding outdoor performance of various PV technologies
- › Demonstrated on a monofacial BIPV façade module (part of PVPS Task15E round robin)
- › Use case comparison of monofacial with bifacial
- › Use case comparison of bifacial full-cells with bifacial half-cells

# INDOOR VS. OUTDOOR DATA COLLECTION

## indoor



- › Matrix according to 61853-1 chapter 8.2 (**indoor**)
- ›  $G_{POA}$  and  $T_{mod}$  are set as close as possible to the values in the matrix
- › IV-flash from above:  $AOI = 90^\circ \rightarrow IAM = 1.0$
- › *Indoor results presented in 6BV.4.7 'BIPV Round Robin Action of IEA PVPS Task15', P.Illich et.al*

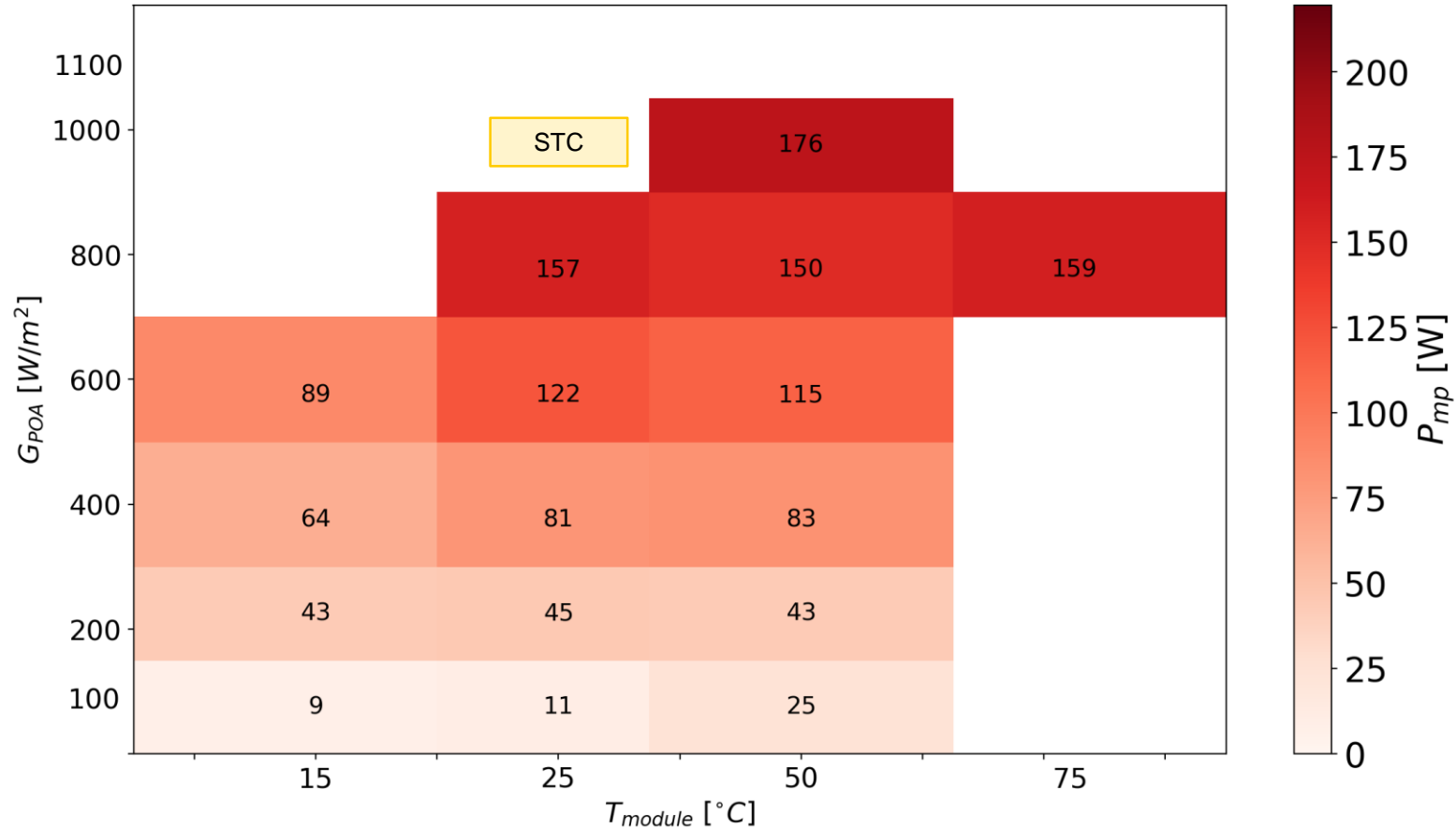
## outdoor

- › Matrix according to 61853-1 chapter 8.4 (**natural sunlight without tracker**) taking all points without restriction of 8.3.2
- › Example of Taks15E round-robin sample (M17-02288)
- › Measurement period = full year (2018-07-01 till 2019-06-29)
- › Recording interval = 1 minute & sampling interval = 5 minutes
- ›  $AOI$  varying  $\rightarrow$   $IAM$  varying

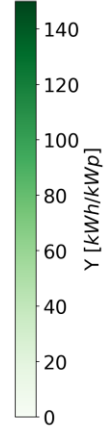
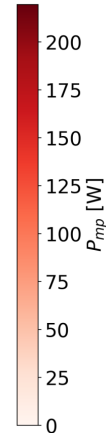
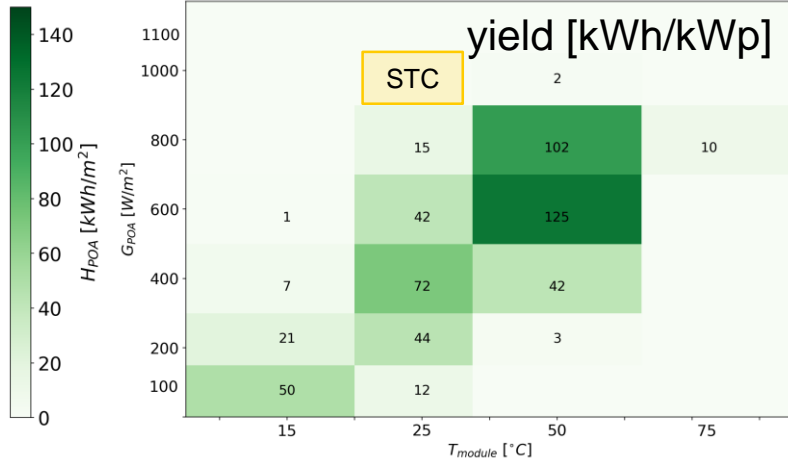
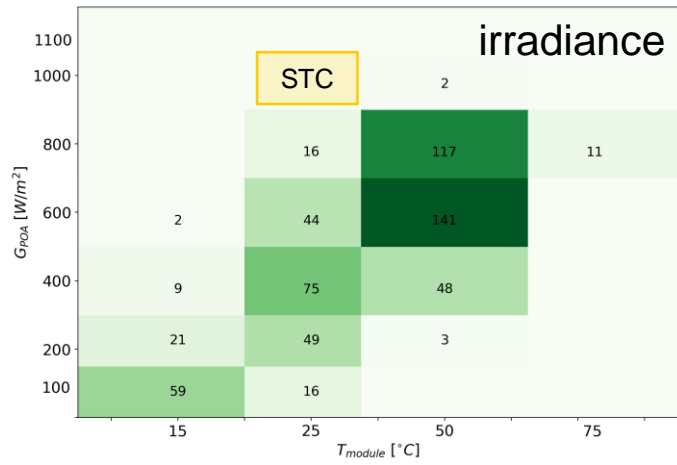
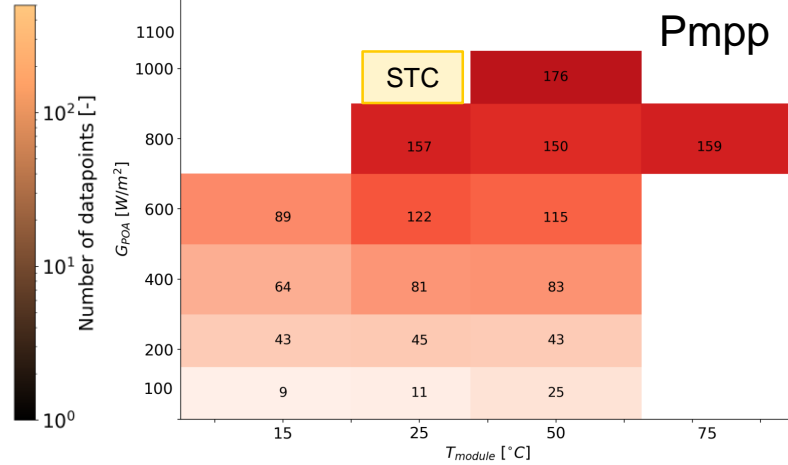
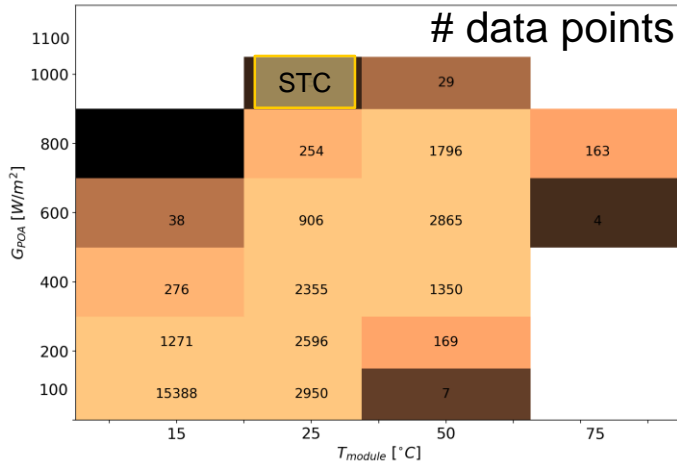
- › *Comparison between Indoor and Outdoor results are part of 2<sup>nd</sup> phase of IEA PVPS Task15', to be published in 2020*



# 1. VISUALIZATION

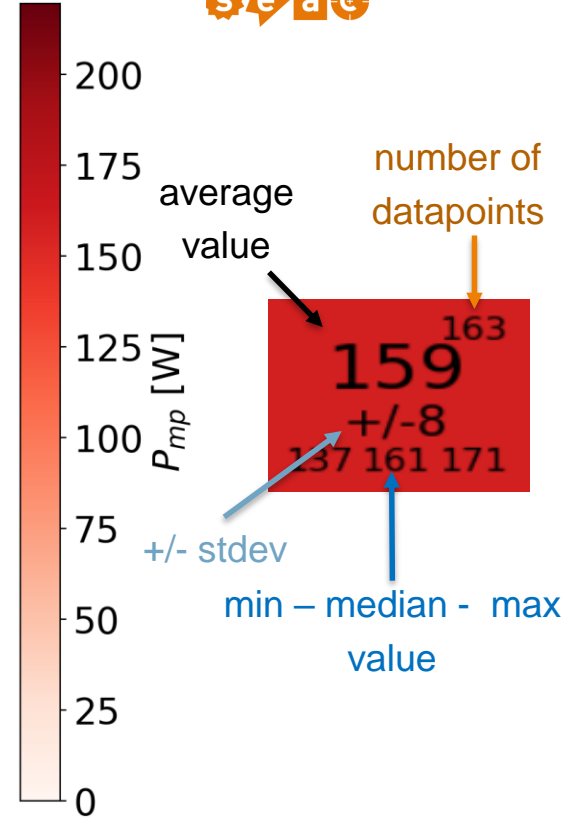
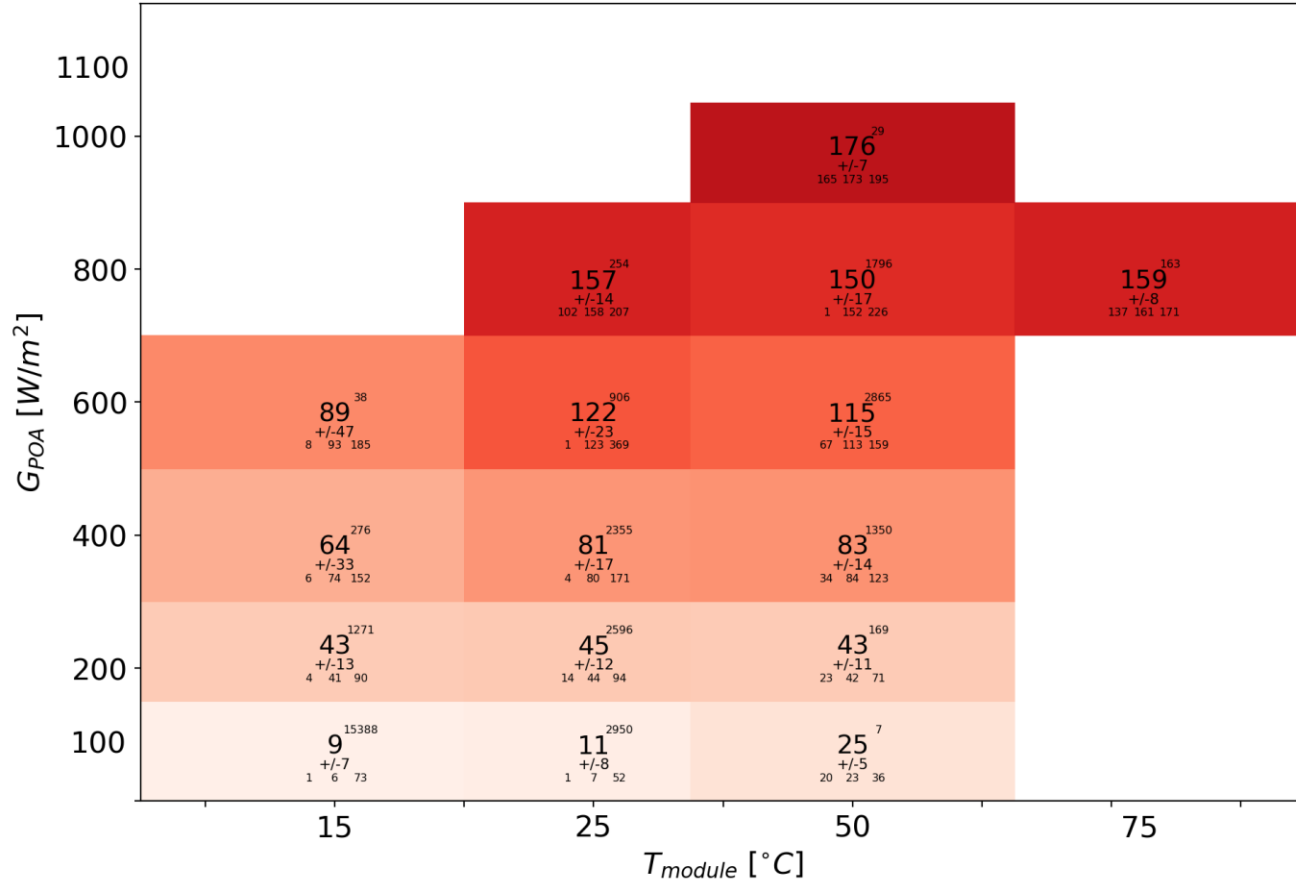


# 2. SIGNIFICANCE OF EACH BIN-POINT



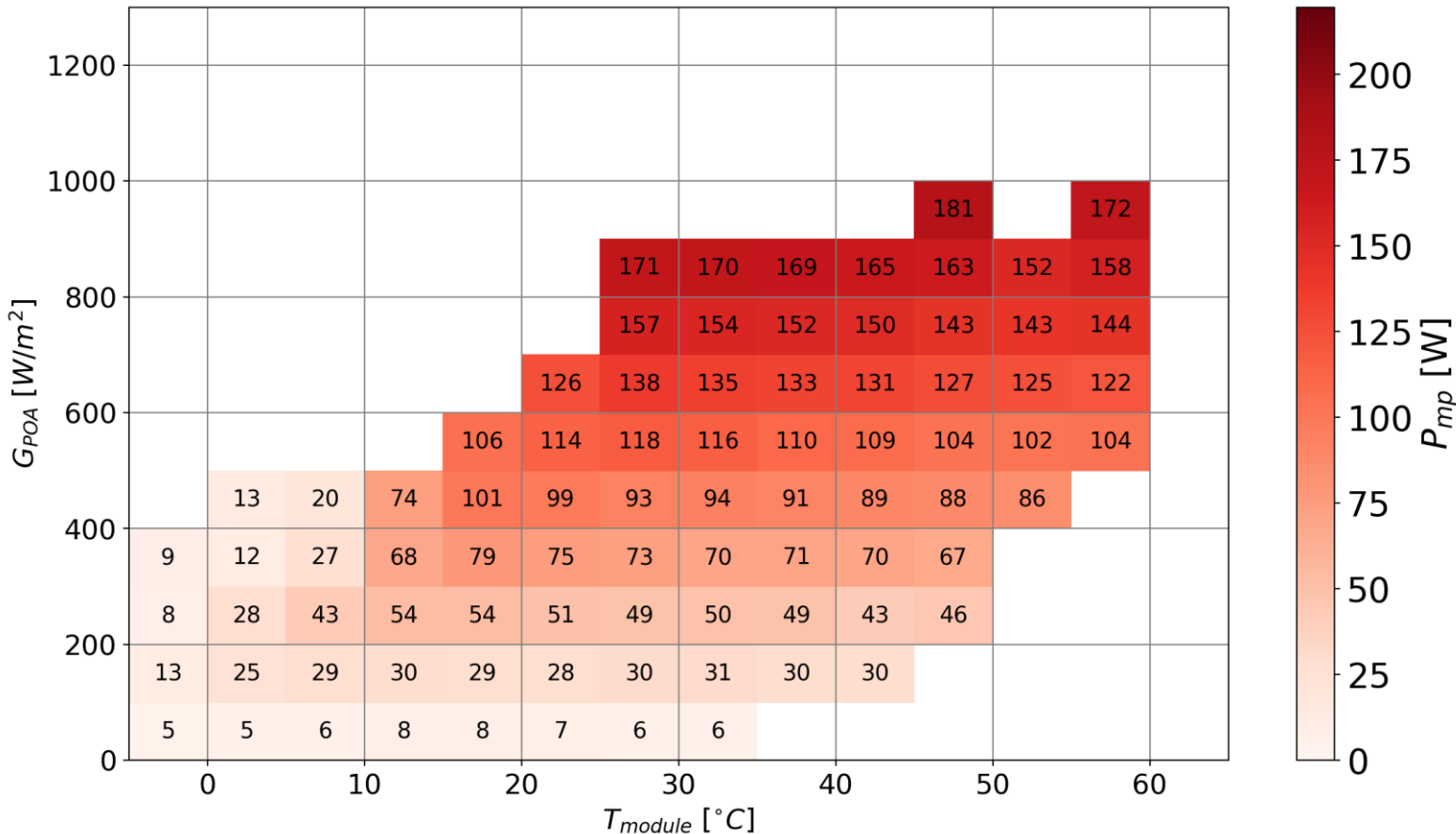
Additional matrices show importance of each bin to total yearly yield

# 3. STATISTICS PER BIN

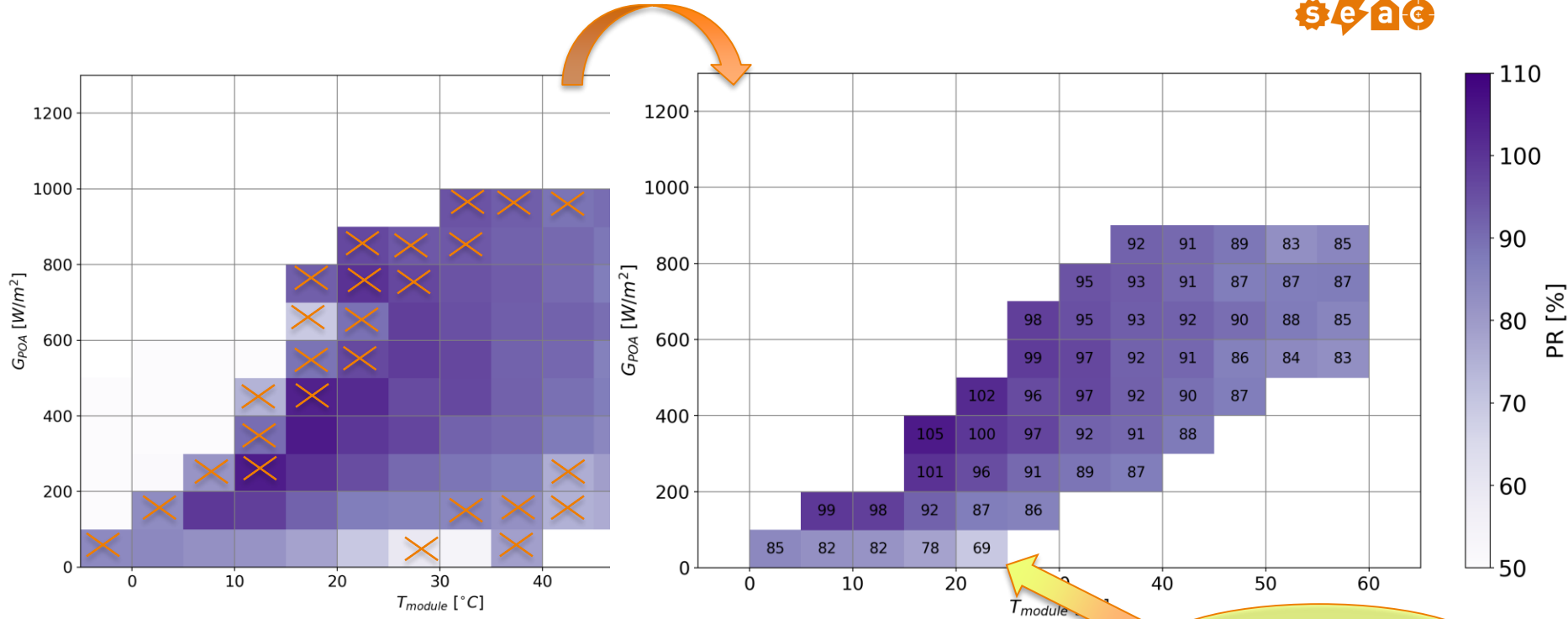




# 4. MORE BINS



# 5. HIDING BINS WITH LOW-SIGNIFICANCE

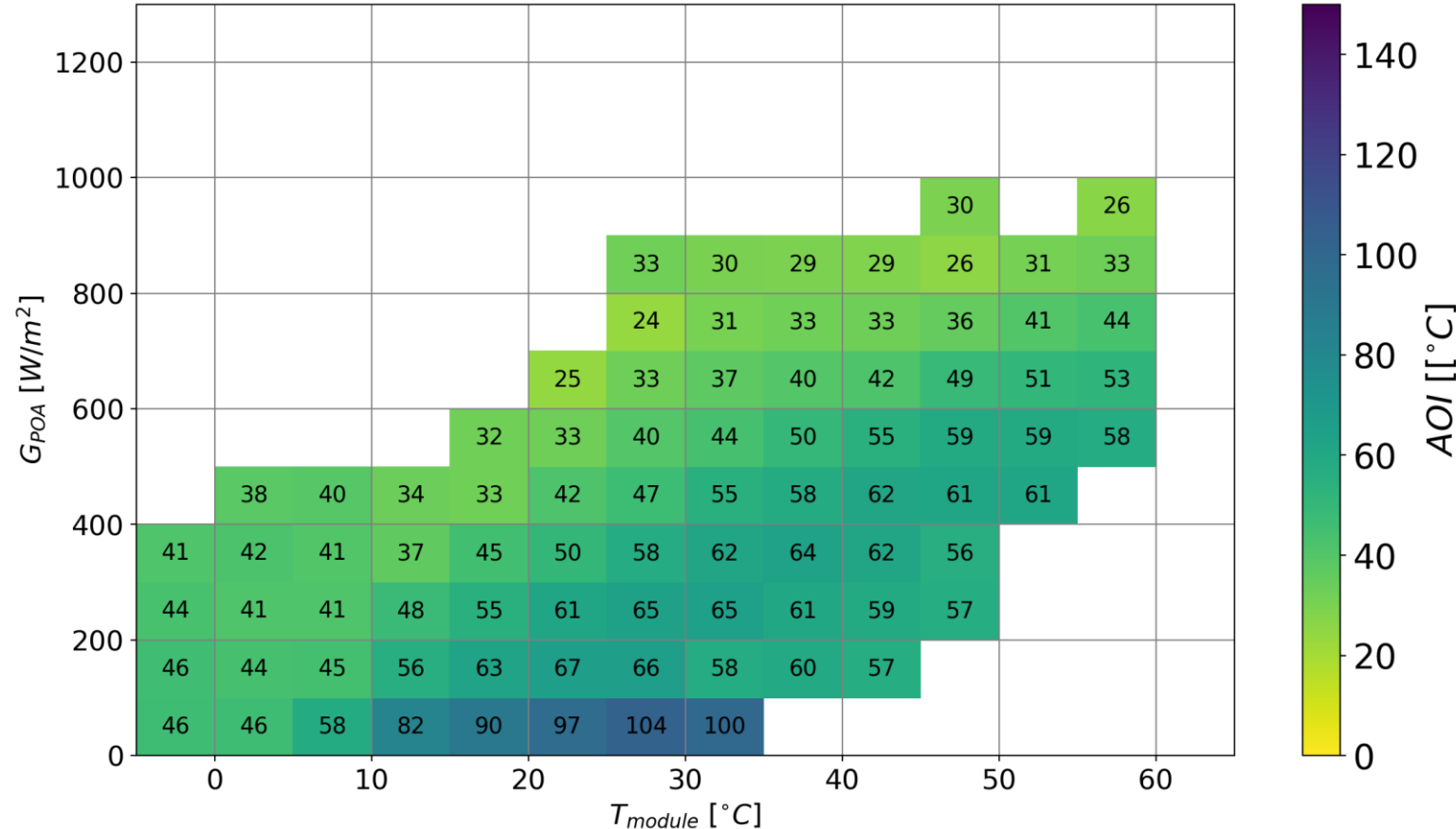


Option to hide bins (discard from visualization) based on criterium:

- Less than x datapoints in bin (x = typical 5)
- Less than y% contribution of yield in bin to total yield (y% = typical 0.5%)

Why such a low PR?

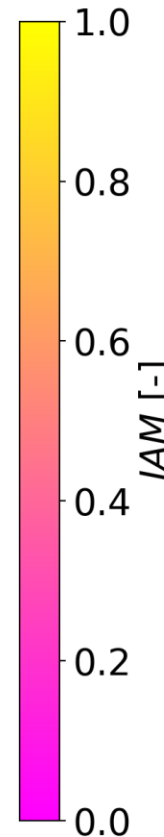
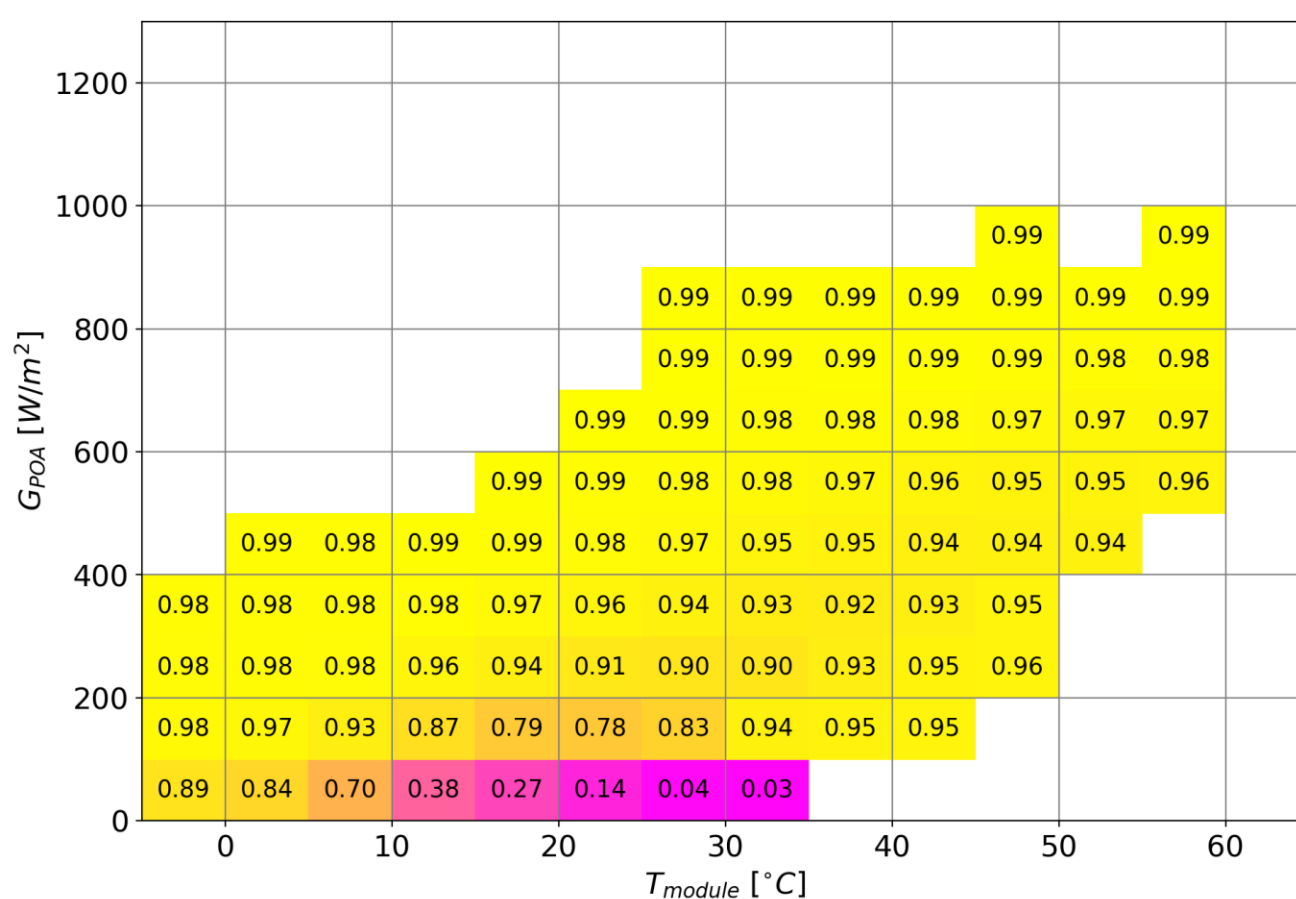
# AOI-EFFECT IN OUTDOOR DATA



outdoor

As expected the higher AOI can be found in the lower irradiance bins.

# IAM-EFFECT IN OUTDOOR



outdoor

The lowest bin ( $G_{POA} < 100$  W/m<sup>2</sup>) is nearly completely 'destroyed' by the IAM-effect!

# EXPERIMENTAL SETUP

- › Rooftop IV-tracing system at ECN.TNO in Petten, the Netherlands
- › Every 10 minutes, simultaneous measurement of all module IV-curves and  $G_{POA}$  and  $T_{mod}$
- › South-facing, 30° tilt
- › Irradiance sensors:
  - ›  $G_{POA}$ : Plane-Of-Array pyranometer and ref cells
  - ›  $G_{BOA}$ : Back of plane reference cells
  - › GHI
  - › Sun trackers for DNI and DHI





# $\Delta PR = \text{DIFFERENCE IN DC PR}$

1300-1400							15%	15%					
1200-1300						13%	17%	11%	23%	2%			
1100-1200					5%	15%	12%	12%	11%	11%	10%	14%	
1000-1100					11%	11%	11%	11%	12%	11%	10%	10%	
900-1000				11%	12%	10%	11%	12%	11%	11%	10%	10%	
800-900			13%	11%	11%	10%	11%	11%	11%	11%	10%	10%	
700-800			12%	12%	12%	11%	11%	12%	12%	11%	11%	11%	
600-700			12%	11%	11%	12%	13%	12%	13%	11%	12%	12%	
500-600			12%	11%	12%	13%	13%	14%	13%	13%	11%		
400-500			11%	11%	12%	14%	14%	14%	14%	16%	15%	16%	
300-400			13%	12%	14%	16%	16%	17%	17%	15%	19%		
200-300		12%	13%	14%	15%	17%	18%	19%	21%	24%			
100-200		15%	15%	16%	18%	19%	22%	37%	29%	28%			
0-100	18%	25%	19%	19%	23%	29%	46%	43%	38%				
	-10	-5	0	5	10	15	20	25	30	35	40	45	50
	-5	0	5	10	15	20	25	30	35	40	45	50	55

- Gain of  $\Delta PR=11\%$  at high irradiance (700-1100  $G_{POA}$ )
- Increasing to  $\Delta PR > 20\%$  gain at low  $G_{POA}$
- Increasing to even higher  $\Delta PR \approx 40\%$  at high  $T_{mod}$  and low  $G_{POA}$ : summer evenings

# PR BASED ON G\_POA (L) AND G\_BIF (R)

- ›  $G_{total} := G_{POA} + G_{BOA}$
- › However, well-known that  $G_{BOA}$  cannot be fully exploited.
- › Assume bifaciality factor = 85%. Then  $G_{BIF} := G_{POA} + 0.85 * G_{BOA}$

Temperature Range (°C)	monofacial n-PERT												
	-10	-5	0	5	10	15	20	25	30	35	40	45	50
1300-1400						81%	90%						
1200-1300						95%	91%	88%	84%	91%			
1100-1200						90%	95%	96%	92%	93%	91%	89%	86%
1000-1100						102%	99%	97%	93%	92%	90%	90%	88%
900-1000					105%	101%	100%	97%	94%	93%	91%	89%	88%
800-900				110%	107%	103%	100%	97%	95%	93%	92%	90%	89%
700-800				109%	106%	103%	100%	98%	96%	94%	92%	91%	88%
600-700			113%	109%	107%	104%	100%	98%	96%	95%	93%	90%	91%
500-600			110%	111%	107%	105%	101%	99%	97%	96%	94%	90%	
400-500			111%	109%	106%	104%	100%	98%	97%	96%	94%	93%	
300-400			110%	107%	105%	101%	99%	98%	97%	96%	95%		
200-300		110%	109%	106%	104%	100%	99%	98%	97%	95%			
100-200		109%	106%	105%	102%	98%	96%	91%	88%	92%			
0-100	104%	107%	104%	101%	97%	94%	94%	89%	91%				

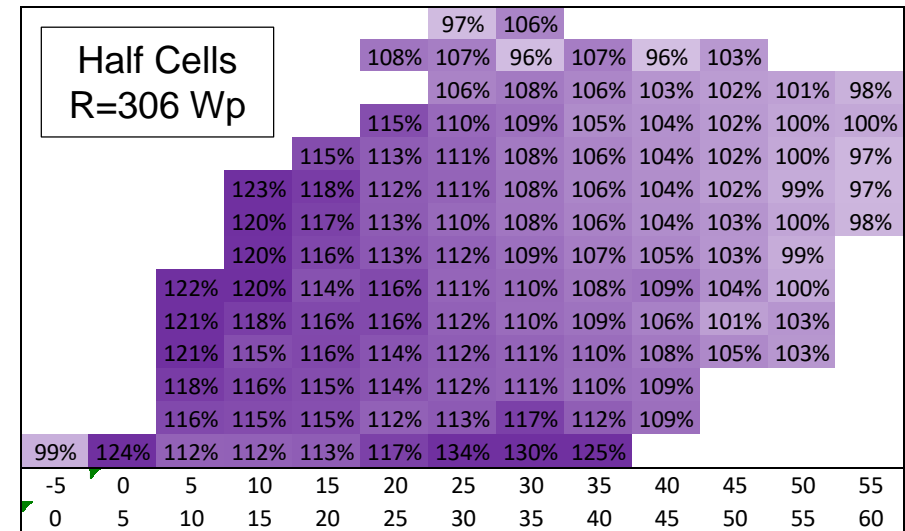
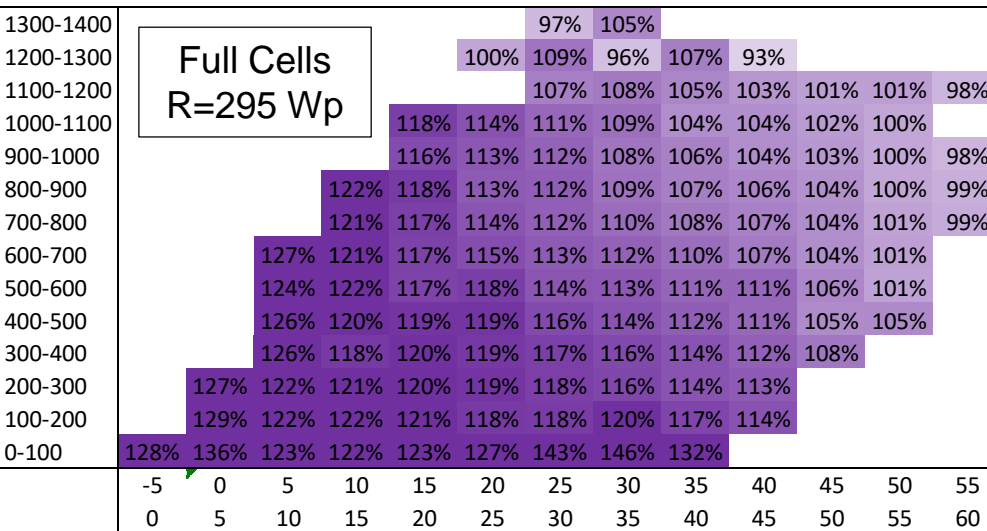
Temperature Range (°C)	bifacial n-PERT												
	-10	-5	0	5	10	15	20	25	30	35	40	45	50
1300-1400													
1200-1300													
1100-1200													
1000-1100													
900-1000													
800-900													
700-800													
600-700													
500-600													
400-500													
300-400													
200-300													
100-200													
0-100													

- › Bifacial DC PR's more/less aligned with normal behaviour (Temperature loss and R series loss)



# USE CASE 2: FULL CELLS VS. HALF CELLS

- › Two bifacial n-PERT modules, left full cell, right half cell
- › Booth glass-glass modules and BoM identical
- › March-Dec 2018, 10 minute IV-tracing, ≈ 20.000 data points after removing sensor failures etc.



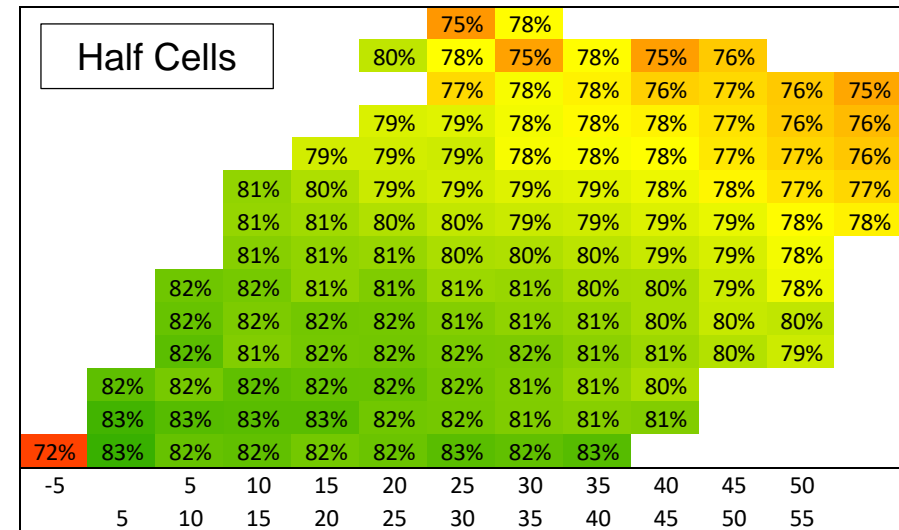
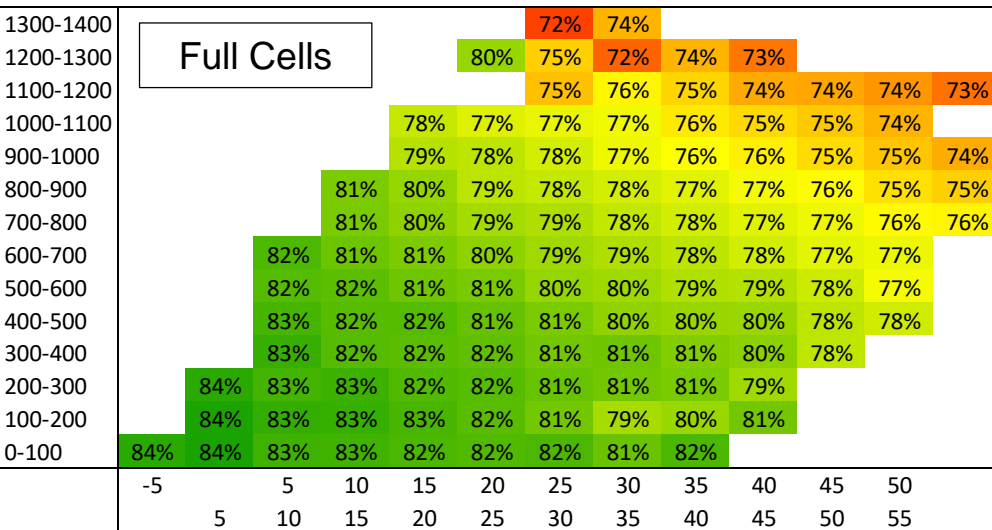
# ΔPR (= HALF CELLS – FULL CELLS)

1300-1400							0%	1%						
1200-1300						9%	-1%	1%	1%	4%				
1100-1200							0%	1%	1%	1%	1%	0%	1%	
1000-1100						2%	1%	0%	1%	0%	1%	1%		
900-1000				1%	0%	0%	0%	0%	0%	0%	0%	0%	0%	0%
800-900		2%	1%	0%	0%	0%	0%	0%	0%	0%	-1%	0%	0%	
700-800		0%	1%	0%	-1%	-1%	-1%	-1%	-1%	0%	0%	0%	-1%	
600-700		0%	0%	-1%	-1%	-2%	-2%	-1%	-1%	-1%	-1%			
500-600	-1%	-1%	-2%	-1%	-2%	-2%	-2%	-2%	-2%	-1%	0%			
400-500	-3%	-2%	-2%	-3%	-3%	-3%	-3%	-3%	-3%	-2%	-1%			
300-400	-4%	-2%	-3%	-4%	-4%	-4%	-3%	-3%	-3%	-2%				
200-300	-4%	-4%	-4%	-4%	-4%	-4%	-4%	-4%	-3%					
100-200	-6%	-6%	-5%	-6%	-4%	-2%	-3%	-4%						
0-100	-28%	-11%	-10%	-10%	-10%	-9%	-7%	-15%	-6%					
	-5	0	5	10	15	20	25	30	35	40	45	50	55	
	0	5	10	15	20	25	30	35	40	45	50	55	60	

Why such a low PR?

# FF FOR FULL CELLS (L) AND HALF CELLS (R)

- › Normal behaviour: at high  $G_{\text{POA}} \Rightarrow$  high  $I_{\text{sc}} \Rightarrow$  high R losses  $\Rightarrow$  low FF
- › And also normal behaviour: at high  $T_{\text{mod}} \Rightarrow$  low V  $\Rightarrow$  low FF



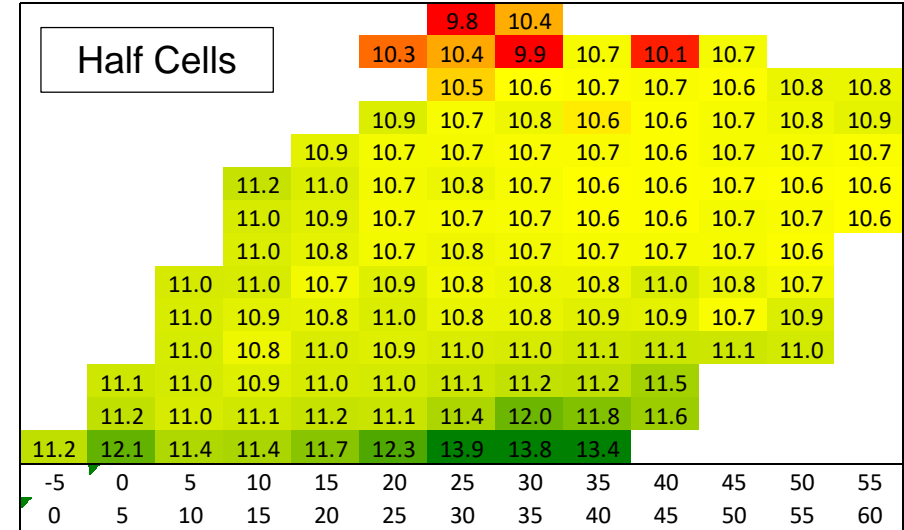
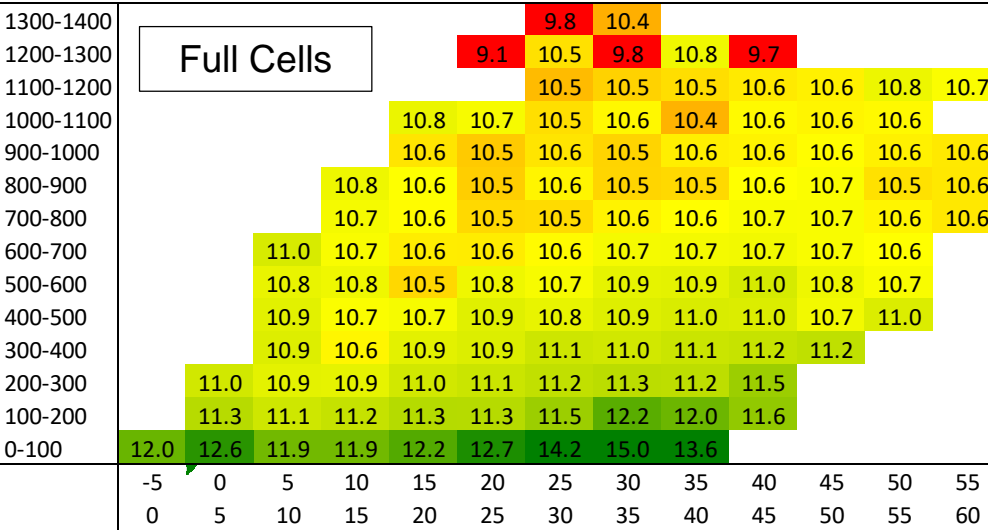
# DIFFERENCE IN FF (HALF CELLS – FULL CELLS)

1300-1400							3%	4%												
1200-1300					0%		3%	3%	3%	2%										
1100-1200							2%	2%	2%	2%	3%	3%	2%							
1000-1100						2%	2%	2%	2%	2%	2%	2%								
900-1000				0%	1%	2%	1%	2%	2%	2%	2%	2%	2%							
800-900			0%	0%	1%	1%	1%	2%	2%	2%	2%	2%	2%							
700-800			0%	0%	1%	1%	1%	2%	2%	2%	2%	2%	2%							
600-700			0%	0%	1%	1%	1%	1%	2%	2%	2%	1%								
500-600			0%	0%	0%	1%	1%	1%	1%	2%	1%	2%								
400-500			0%	0%	0%	0%	1%	1%	1%	1%	1%	2%								
300-400			-1%	-1%	0%	0%	1%	0%	1%	0%	2%									
200-300		-1%	-1%	-1%	0%	0%	0%	0%	0%	1%										
100-200		-1%	-1%	-1%	0%	0%	1%	2%	2%	0%										
0-100		-1%	-1%	0%	-1%	0%	0%	1%	0%											
	-5	5	10	15	20	25	30	35	40	45	50									
	0	5	10	15	20	25	30	35	40	45	50	55								

Nothing really significant in this  $\Delta FF$ .

What is happening at low  $G_{POA}$ ?

# I\_SC DIVIDED BY G\_POA



Equal or Different ? See next slide.

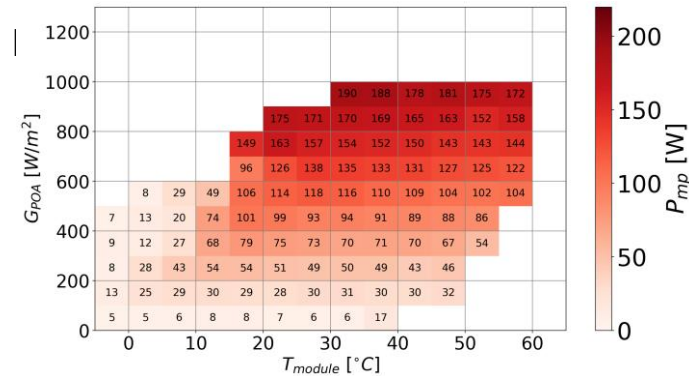
# DIFFERENCE IN (BIFACIAL) $I_{SC}/G_{POA}$

1300-1400							-0.1	0.0					
1200-1300						1.2	-0.1	0.1	-0.1	0.3			
1100-1200							0.1	0.1	0.1	0.1	0.1	0.0	0.2
1000-1100					0.3	0.1	0.2	0.1	0.0	0.1	0.2		
900-1000			0.3	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.1	
800-900		0.4	0.3	0.2	0.2	0.2	0.1	0.0	0.0	0.0	0.1	0.1	
700-800		0.3	0.3	0.2	0.2	0.1	0.0	0.0	0.0	0.0	0.1	0.1	
600-700		0.3	0.3	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0		
500-600	0.2	0.2	0.2	0.2	0.1	-0.1	-0.1	0.0	0.0	0.1			
400-500	0.1	0.2	0.1	0.1	0.0	-0.1	-0.1	-0.1	-0.1	0.0			
300-400	0.1	0.2	0.1	0.0	-0.1	-0.1	-0.1	0.0	-0.1				
200-300	0.0	0.1	0.1	-0.1	-0.1	-0.1	-0.1	0.0	-0.1				
100-200	-0.1	-0.1	-0.1	-0.1	-0.2	-0.2	-0.2	-0.2	-0.1				
0-100	-0.6	-0.6	-0.5	-0.5	-0.5	-0.3	-1.2	-0.2					
	-5	0	5	10	15	20	25	30	35	40	45	50	55
	0	5	10	15	20	25	30	35	40	45	50	55	60

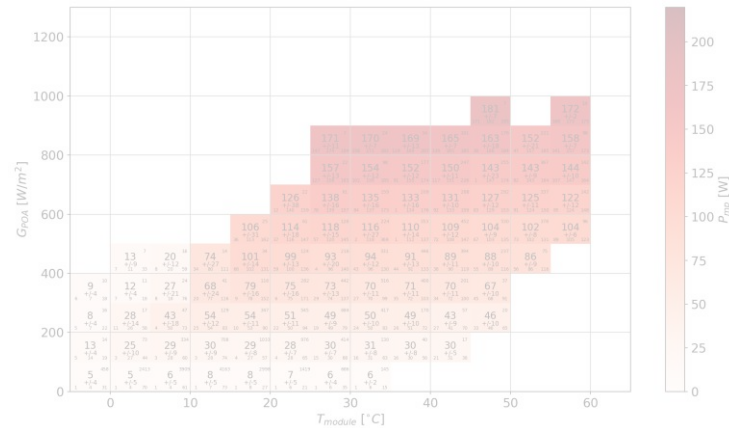
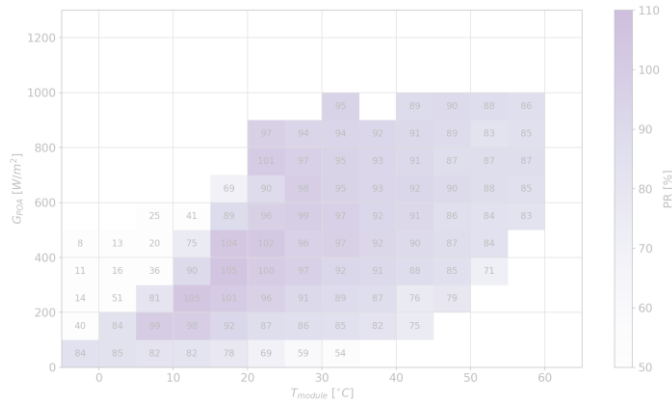
- › Found root cause ! Clearly drop in  $I_{sc}/G_{POA}$  for half-cells at lower irradiance.
- › Damages due to cutting increase recombination. At low irradiance (low injection) most sensitive.

## 61853-MATRIX STYLE IS PERFECT TOOL FOR RESEARCH ON PV TECHNOLOGIES

- › Making the 7x4 matrix more fine with 100 W/m<sup>2</sup> and 5°C bins.
- › Plotting not only  $P_{MPP}$ , but any PV-panel parameter (e.g.  $V_{OC}$ ,  $V_{MPP}$ , |PR).
- › Analyzing statistics per bin is a tool for cleaning outdoor data.
- › Presented use cases:
  1. Comparison of monofacial with bifacial:
    - $\Delta PR$  gain highest for low  $G_{POA}$
    - For bifi: PR-matrix based on  $G_{BIF}$  looks similar to mono PR-matrix.
    - Hence irradiance boost at low  $G_{POA}$
  2. Comparison of bifacial full-cells with bifacial half-cells:
    - $\Delta PR$  drop for low  $G_{POA}$  for half-cells not caused by FF (?)
    - Root cause found in  $\Delta (I_{sc}/G_{POA})$ -matrix! Effect attributed to cutting losses



# THE REFINED 61853-MATRIX IS THE TOOL FOR ENERGY RATING AND ANALYSIS OF PV TECHNOLOGIES, LIKE BIFACIAL



**THANK YOU FOR YOUR ATTENTION**