#### APPLICATION OF IEC 61853 MATRIX TO BIFACIAL PV

#### **Roland Valckenborg and Bas van Aken**



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#### History:

- > STC most important, and longest history in PV world.
- Additional parameters (e.g. NOCT) introduced in last couple of decades.

#### Is it possible to calculate the full year yield based on these datasheet value ?

#### New 61853 defines 7 $G_{POA} \times 4 T_{mod}$ matrix, leaving out the non-existing points:

Irradiance	Spectrum		M	odule temperature	
W·m <sup>−2</sup>		15 °C	25 °C	50 °C	75 °C
1 100	AM1,5	NA			1.1.1.1
1 000	AM1,5		STC		
800	AM1,5				
600	AM1,5				
400	AM1,5				NA
200	AM1,5			NA	NA
100	AM1,5			NA	NA

## **INTRODUCTION 'THE IEC-61853 MATRIX'**

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- > Objective of 61853: **Testing and rating** of a PV-module (under well-defined climatic conditions)
  - Part 1: Irradiance and Temperature performance measurements and power rating
  - > Part 2: Spectral responsivity, incidence angle, and module operating temperature
  - Part 3: Calculation of Energy Rating of PV modules
  - > Part 4: Standard Reference Climatic Profiles
- Spectral-effects are described also in 61853:2, but less important than the matrix  $\rightarrow$  Future work

### **OUTLINE PRESENTATION**

- > Our contribution:
  - > additional visualization and statistics
  - > for the **Research Purpose** of understanding outdoor performance of various PV technologies

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- > Demonstrated on a monofacial BIPV façade module (part of PVPS Task15E round robin)
- > Use case comparison of monofacial with bifacial
- > Use case comparison of bifacial full-cells with bifacial half-cells

## **INDOOR VS. OUTDOOR DATA COLLECTION**



- Matrix according to 61853-1 chapter 8.2 (indoor)
- G<sub>POA</sub> and T<sub>mod</sub> are set as close as possible to the values in the matrix
- V IV-flash from above: AOI =  $90^{\circ} \rightarrow IAM = 1.0$

indoor

Indoor results presented in 6BV.4.7 'BIPV Round Robin Action of IEA PVPS Task15', P.IIIich et.al outdoor

Matrix according to 61853-1 chapter 8.4 (natural sunlight without tracker) taking all points without restriction of 8.3.2

Example of Taks15E round-robin sample (M17-02288)

- Measurement period = full year (2018-07-01 till 2019-06-29)
- Recording interval = 1 minute & sampling interval = 5 minutes
- > AOI varying  $\rightarrow$  IAM varying



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Comparison between Indoor and Outdoor results are part of 2<sup>nd</sup> phase of IEA PVPS Task15', to be published in 2020

#### **1. VISUALIZATION**



## **2. SIGNIFICANCE OF EACH BIN-POINT**



#### **3. STATISTICS PER BIN**









#### **4. MORE BINS**



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#### **5. HIDING BINS WITH LOW-SIGNIFICANCE**



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- Less than x datapoints in bin (x = typical 5)
- Less than y% contribution of yield in bin to total yield (y% = typical 0.5%) •

#### **AOI-EFFECT IN OUTDOOR DATA**





#### **IAM-EFFECT IN OUTDOOR**



#### **EXPERIMENTAL SETUP**

- > Rooftop IV-tracing system at ECN.TNO in Petten, the Netherlands
- > Every 10 minutes, simultaneuos measurement of all module IV-curves and G<sub>POA</sub> and T<sub>mod</sub>
- South-facing, 30° tilt
- Irradiance sensors:
  - G<sub>POA</sub>: Plane-Of-Array pyranometer and ref cells
  - G<sub>BOA</sub>: Back of plane reference cells
  - ) GHI
  - > Sun trackers for DNI and DHI



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#### **USE CASE 1: MONOFACIAL VS. BIFACIAL**

- > Two n-PERT modules, left white back sheet, right glass-glass
- March-Dec 2018, 10 minute IV-tracing, ≈ 20.000 data points after removing sensor failures etc.
- > DC PR based on G<sub>POA</sub>

1300-1400							81%	90%												96%	105%					
1200-1300	l n	nono	facia	al		95%	91%	88%	84%	91%					bifa	cial			109%	108%	99%	107%	94%			
1100-1200			=PT			90%	95%	96%	92%	93%	91%	89%	86%		n DI	DT			96%	110%	108%	104%	103%	102%	99%	100%
1000-1100		11-r L	_1\1			102%	99%	97%	93%	92%	90%	90%	88%						113%	110%	108%	104%	104%	102%	100%	98%
900-1000					105%	101%	100%	97%	94%	93%	91%	89%	88%					116%	113%	110%	107%	106%	104%	102%	100%	97%
800-900				110%	107%	103%	100%	97%	95%	93%	92%	90%	89%				123%	119%	114%	110%	108%	107%	105%	103%	100%	99%
700-800				109%	106%	103%	100%	98%	96%	94%	92%	91%	88%				120%	118%	114%	111%	109%	108%	106%	103%	102%	99%
600-700			113%	109%	107%	104%	100%	98%	96%	95%	93%	90%	91%				121%	118%	115%	112%	111%	109%	107%	104%	103%	102%
500-600			110%	111%	107%	105%	101%	99%	97%	96%	94%	90%					123%	118%	116%	114%	111%	111%	109%	106%	101%	
400-500			111%	109%	106%	104%	100%	98%	97%	96%	94%	93%				121%	120%	118%	117%	114%	113%	112%	112%	109%	109%	
300-400			110%	107%	105%	101%	99%	98%	97%	96%	95%					122%	120%	120%	117%	115%	115%	114%	111%	114%		
200-300		110%	109%	106%	104%	100%	99%	98%	97%	95%					121%	122%	120%	119%	117%	116%	117%	118%	119%			
100-200		109%	106%	105%	102%	98%	96%	91%	88%	92%					124%	121%	121%	120%	117%	119%	128%	117%	120%			
0-100	104%	107%	104%	101%	97%	94%	94%	89%	91%					122%	132%	122%	120%	120%	124%	140%	132%	129%				
	-10	-5	0	5	10	15	20	25	30	35	40	45	50	-10	-5	0	5	10	15	20	25	30	35	40	45	50
	-5	0	5	10	15	20	25	30	35	40	45	50	55	-5	0	5	10	15	20	25	30	35	40	45	50	55

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#### $\triangle PR = DIFFERENCE IN DC PR$

1300-1400							15%	15%					
1200-1300						13%	17%	11%	23%	2%			
1100-1200						5%	15%	12%	12%	11%	11%	10%	14%
1000-1100						11%	11%	11%	11%	12%	11%	10%	10%
900-1000					11%	12%	10%	11%	12%	11%	11%	10%	10%
800-900				13%	11%	11%	10%	11%	11%	11%	11%	10%	10%
700-800				12%	12%	12%	11%	11%	12%	12%	11%	11%	11%
600-700				12%	11%	11%	12%	13%	12%	13%	11%	12%	12%
500-600				12%	11%	12%	13%	13%	14%	13%	13%	11%	
400-500			11%	11%	12%	14%	14%	14%	14%	16%	15%	16%	
300-400			13%	12%	14%	16%	16%	17%	17%	15%	19%		
200-300		12%	13%	14%	15%	17%	18%	19%	21%	24%			
100-200		15%	15%	16%	18%	19%	22%	37%	29%	28%			
0-100	18%	25%	19%	19%	23%	29%	46%	43%	38%				
	-10	-5	0	5	10	15	20	25	30	35	40	45	50
	-5	0	5	10	15	20	25	30	35	40	45	50	55

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- Gain of  $\triangle PR=11\%$  at high irradiance (700-1100 G<sub>POA</sub>)
- Increasing to  $\Delta PR > 20\%$  gain at low G<sub>POA</sub>
- Increasing to even higher  $\Delta PR \approx 40\%$  at high  $T_{mod}$  and low  $G_{POA}$ : summer evenings



$$G_{\text{total}} := G_{\text{POA}} + G_{\text{BOA}}$$

- However, well-known that G<sub>BOA</sub> cannot be fully exploited.
- Assume bifaciality factor = 85%. Then  $G_{BIF} := G_{POA} + 0.85 * G_{BOA}$

L300-1400							81%	90%											96%	96%	94%	95%	90%			
L200-1300	l m	nono	facia	al		95%	91%	88%	84%	91%					bifa	cial			89%	99%	96%	92%	91%	91%	89%	90%
100-1200			DT			90%	95%	96%	92%	93%	91%	89%	86%						101%	98%	97%	93%	94%	92%	90%	88%
L000-1100		11-F				102%	99%	97%	93%	92%	90%	90%	88%		11-PI			102%	100%	98%	96%	95%	93%	92%	90%	88%
900-1000					105%	101%	100%	97%	94%	93%	91%	89%	88%				108%	105%	101%	98%	96%	95%	93%	92%	90%	88%
300-900				110%	107%	103%	100%	97%	95%	93%	92%	90%	89%				105%	104%	100%	98%	96%	95%	94%	92%	91%	88%
700-800				109%	106%	103%	100%	98%	96%	94%	92%	91%	88%				105%	104%	101%	98%	97%	95%	94%	91%	90%	89%
500-700			113%	109%	107%	104%	100%	98%	96%	95%	93%	90%	91%				106%	103%	101%	98%	96%	95%	94%	91%	88%	
500-600			110%	111%	107%	105%	101%	99%	97%	96%	94%	90%				107%	105%	102%	100%	97%	95%	95%	95%	92%	91%	
100-500			111%	109%	106%	104%	100%	98%	97%	96%	94%	93%				105%	104%	101%	98%	96%	95%	93%	89%	93%	92%	
300-400			110%	107%	105%	101%	99%	98%	97%	96%	95%				106%	103%	102%	99%	96%	94%	94%	93%	92%	92%		
200-300		110%	109%	106%	104%	100%	99%	98%	97%	95%					102%	102%	99%	96%	94%	92%	90%	88%	85%			
L00-200		109%	106%	105%	102%	98%	96%	91%	88%	92%					103%	100%	97%	94%	88%	84%	81%	77%				
0-100	104%	107%	104%	101%	97%	94%	94%	89%	91%					98%	99%	98%	94%	89%	84%	77%	75%	76%				
	-10	-5	0	5	10	15	20	25	30	35	40	45	50	-10	-5	0	5	10	15	20	25	30	35	40	45	50
	-5	0	5	10	15	20	25	30	35	40	45	50	55	-5	0	5	10	15	20	25	30	35	40	45	50	55

Bifacial DC PR's more/less aligned with normal behaviour (Temperature loss and R series loss)

#### **USE CASE 2: FULL CELLS VS. HALF CELLS**

- > Two bifacial n-PERT modules, left full cell, right half cell
- > Booth glass-glass modules and BoM identical
- March-Dec 2018, 10 minute IV-tracing,  $\approx$  20.000 data points after removing sensor failures etc.

1300-1400							97%	105%												97%	106%					
1200-1300		Full (	Cells	S		100%	109%	96%	107%	93%				F	Half	Cells	S		108%	107%	96%	107%	96%	103%		
1100-1200			Б \//	n			107%	108%	105%	103%	101%	101%	98%		2∩	6 111	n			106%	108%	106%	103%	102%	101%	98%
1000-1100		~=29	5 00	ρ	118%	114%	111%	109%	104%	104%	102%	100%			-30	0 00	μ		115%	110%	109%	105%	104%	102%	100%	100%
900-1000					116%	113%	112%	108%	106%	104%	103%	100%	98%					115%	113%	111%	108%	106%	104%	102%	100%	97%
800-900				122%	118%	113%	112%	109%	107%	106%	104%	100%	99%				123%	118%	112%	111%	108%	106%	104%	102%	99%	97%
700-800				121%	117%	114%	112%	110%	108%	107%	104%	101%	99%				120%	117%	113%	110%	108%	106%	104%	103%	100%	98%
600-700			127%	121%	117%	115%	113%	112%	110%	107%	104%	101%					120%	116%	113%	112%	109%	107%	105%	103%	99%	
500-600			124%	122%	117%	118%	114%	113%	111%	111%	106%	101%				122%	120%	114%	116%	111%	110%	108%	109%	104%	100%	
400-500			126%	120%	119%	119%	116%	114%	112%	111%	105%	105%				121%	118%	116%	116%	112%	110%	109%	106%	101%	103%	
300-400			126%	118%	120%	119%	117%	116%	114%	112%	108%					121%	115%	116%	114%	112%	111%	110%	108%	105%	103%	
200-300		127%	122%	121%	120%	119%	118%	116%	114%	113%						118%	116%	115%	114%	112%	111%	110%	109%			
100-200		129%	122%	122%	121%	118%	118%	120%	117%	114%						116%	115%	115%	112%	113%	117%	112%	109%			
0-100	128%	136%	123%	122%	123%	127%	143%	146%	132%					99%	124%	112%	112%	113%	117%	134%	130%	125%				
	-5	0	5	10	15	20	25	30	35	40	45	50	55	-5	0	5	10	15	20	25	30	35	40	45	50	55
	0	5	10	15	20	25	30	35	40	45	50	55	60	0	5	10	15	20	25	30	35	40	45	50	55	60

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#### △PR (= HALF CELLS – FULL CELLS)

0

5

10

15

20

25

30

35

40

45

**\$@a@** 1300-1400 0% 1% 1200-1300 -1% 1% 4% 9% 1% 1100-1200 0% 1% 1% 1% 1% 0% 1% 1000-1100 2% 1% 0% 1% 0% 1% 1% 900-1000 1% 0% 0% 0% 0% 0% 0% 0% 0% 800-900 2% 1% 0% 0% 0% 0% 0% 0% 0% -1% 700-800 0% 1% 0% -1% -1% -1% -1% 0% 0% -1% 600-700 0% 0% -1% -1% -2% -2% -1% -1% -1% 500-600 -1% -2% -2% -2% -2% -2% 0% -1% -1% -1% 400-500 -3% -2% -2% -3% -3% -3% -3% -3% -2% -1% 300-400 -4% -2% -3% -4% -4% -3% -3% -2% -4% 200-300 -4% -4% -4% -4% -4% -4% -4% -3% 100-200 -6% -6% -5% -6% -4% -2% -3% -4% 0-100 -28% -11% -10% -10% -10% -9% -7% -15% -6% -5 5 10 15 20 25 30 35 40 45 50 55 0

50 55

<sup>60</sup> Why such a low PR?

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#### FF FOR FULL CELLS (L) AND HALF CELLS (R)

Normal behaviour: at high G<sub>POA</sub> => high I<sub>sc</sub> => high R losses => low FF

And also normal behaviour: at high T<sub>mod</sub> => low V => low FF

1300-1400							72%	74%						1							75%	78%					
1200-1300		Full (	Cells	S		80%	75%	72%	74%	73%					H	Half	Cells	S		80%	78%	75%	78%	75%	76%		
1100-1200							75%	76%	75%	74%	74%	74%	73%								77%	78%	78%	76%	77%	76%	75%
1000-1100					78%	77%	77%	77%	76%	75%	75%	74%								79%	79%	78%	78%	78%	77%	76%	76%
900-1000					79%	78%	78%	77%	76%	76%	75%	75%	74%						79%	79%	79%	78%	78%	78%	77%	77%	76%
800-900				81%	80%	79%	78%	78%	77%	77%	76%	75%	75%					81%	80%	79%	79%	79%	79%	78%	78%	77%	77%
700-800				81%	80%	79%	79%	78%	78%	77%	77%	76%	76%					81%	81%	80%	80%	79%	79%	79%	79%	78%	78%
600-700			82%	81%	81%	80%	79%	79%	78%	78%	77%	77%						81%	81%	81%	80%	80%	80%	79%	79%	78%	
500-600			82%	82%	81%	81%	80%	80%	79%	79%	78%	77%					82%	82%	81%	81%	81%	81%	80%	80%	79%	78%	
400-500			83%	82%	82%	81%	81%	80%	80%	80%	78%	78%					82%	82%	82%	82%	81%	81%	81%	80%	80%	80%	
300-400			83%	82%	82%	82%	81%	81%	81%	80%	78%						82%	81%	82%	82%	82%	82%	81%	81%	80%	79%	
200-300		84%	83%	83%	82%	82%	81%	81%	81%	79%						82%	82%	82%	82%	82%	82%	81%	81%	80%			
100-200		84%	83%	83%	83%	82%	81%	79%	80%	81%						83%	83%	83%	83%	82%	82%	81%	81%	81%			
0-100	84%	84%	83%	83%	82%	82%	82%	81%	82%						72%	83%	82%	82%	82%	82%	83%	82%	83%				
	-5		5	10	15	20	25	30	35	40	45	50			-5		5	10	15	20	25	30	35	40	45	50	
		5	10	15	20	25	30	35	40	45	50	55				5	10	15	20	25	30	35	40	45	50	55	

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## DIFFERENCE IN FF (HALF CELLS – FULL CELLS)

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1300-1400							3%	4%					
1200-1300						0%	3%	3%	3%	2%			
1100-1200							2%	2%	2%	2%	3%	3%	2%
1000-1100						2%	2%	2%	2%	2%	2%	2%	
900-1000					0%	1%	2%	1%	2%	2%	2%	2%	2%
800-900				0%	0%	1%	1%	1%	2%	2%	2%	2%	2%
700-800				0%	0%	1%	1%	1%	2%	2%	2%	2%	2%
600-700				0%	0%	1%	1%	1%	1%	2%	2%	1%	
500-600			0%	0%	0%	1%	1%	1%	1%	2%	1%	2%	
400-500			0%	0%	0%	0%	1%	1%	1%	1%	1%	2%	
300-400			-1%	-1%	0%	0%	1%	0%	1%	0%	2%		-
200-300		-1%	-1%	-1%	0%	0%	0%	0%	0%	1%			
100-200		-1%	-1%	-1%	0%	0%	1%	2%	2%	0%		N	othing really significant
0-100		-1%	-1%	0%	-1%	0%	0%	1%	0%				in this AFF
	-5		5	10	15	20	25	30	35	40	45	50	
	0	5	10	15	20	25	30	35	40	45	50	55	What is happening at
													IOW G <sub>POA</sub> ?

#### I\_SC DIVIDED BY G\_POA

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**SØae** 



> Equal or Different ? See next slide.

## **DIFFERENCE IN (BIFACIAL) I\_SC/G\_POA**

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**SØaG** 

1300-1400							-0.1	0.0					
1200-1300						1.2	-0.1	0.1	-0.1	0.3			
1100-1200							0.1	0.1	0.1	0.1	0.1	0.0	0.2
1000-1100						0.3	0.1	0.2	0.1	0.0	0.1	0.2	
900-1000					0.3	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.1
800-900				0.4	0.3	0.2	0.2	0.2	0.1	0.0	0.0	0.1	0.1
700-800				0.3	0.3	0.2	0.2	0.1	0.0	0.0	0.0	0.1	0.1
600-700				0.3	0.3	0.2	0.2	0.0	0.0	0.0	0.0	0.0	
500-600			0.2	0.2	0.2	0.2	0.1	-0.1	-0.1	0.0	0.0	0.1	
400-500			0.1	0.2	0.1	0.1	0.0	-0.1	-0.1	-0.1	-0.1	0.0	
300-400			0.1	0.2	0.1	0.0	-0.1	-0.1	-0.1	0.0	-0.1		
200-300		0.0	0.1	0.1	-0.1	-0.1	-0.1	-0.1	0.0	-0.1			
100-200		-0.1	-0.1	-0.1	-0.1	-0.2	-0.2	-0.2	-0.2	-0.1			
0-100		-0.6	-0.6	-0.5	-0.5	-0.5	-0.3	-1.2	-0.2				
	-5	0	5	10	15	20	25	30	35	40	45	50	55
	0	5	10	15	20	25	30	35	40	45	50	55	60

Found root cause ! Clearly drop in I<sub>sc</sub>/G<sub>POA</sub> for half-cells at lower irradiance.

> Damages due to cutting increase recombination. At low irradiance (low injection) most sensitive.

#### CONCLUSION

# 61853-MATRIX STYLE IS PERFECT TOOL FOR RESEARCH ON PV TECHNOLOGIES

- Making the 7x4 matrix more fine with 100 W/m<sup>2</sup> and 5°C bins.
- Plotting not only P<sub>MPP</sub>, but any PV-panel parameter (e.g. V<sub>OC</sub>, V<sub>MPP</sub>, | PR).
- > Analyzing statistics per bin is a tool for cleaning outdoor data.
- > Presented use cases:
  - 1. Comparison of monofacial with bifacial:
    - $\Delta PR$  gain highest for low  $G_{POA}$
    - For bifi: PR-matrix based on G<sub>BIF</sub> looks similar to mono PR-matrix.
    - Hence irradiance boost at low G<sub>POA</sub>
  - 2. Comparison of bifacial full-cells with bifacial half-cells:
    - $\Delta PR$  drop for low G<sub>POA</sub> for half-cells not caused by FF (?)
    - Root cause found in  $\Delta$  (I<sub>sc</sub>/G<sub>POA</sub>)-matrix! Effect attributed to cutting losses



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## THE REFINED 61853-MATRIX IS THE TOOL FOR <u>ENERGY RATING AND ANALYSIS</u> OF PV TECHNOLOGIES, LIKE BIFACIAL



**THANK YOU FOR YOUR ATTENTION**