



Challenges and Opportunities in Widespread Bifacial PV Adoption Utility-scale solar development in 2020

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AGENDA: OVERVIEW



- IEC efforts in standardization of bifacial performance monitoring & performance testing
- B Bifacial performance models and parametric sensitivities
- C Project economics and optimization of system design

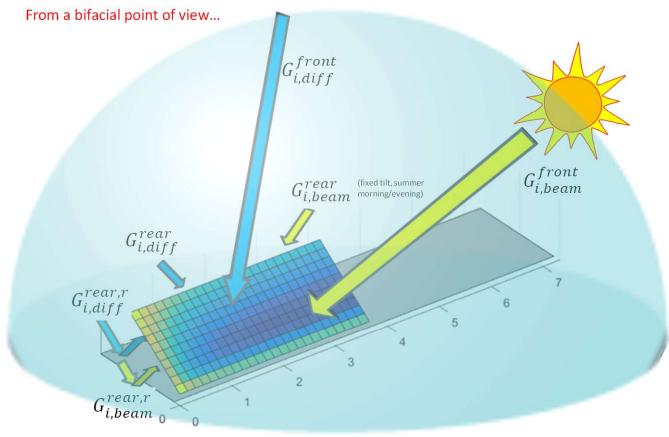








AN OVERVIEW OF THE SOLAR RESOURCE





IEC TS 60904-1-2 (WG2, TC82)

first Bifacial related technical specification, published 01/2019

$$G_{E_i} = 1\ 000\ Wm^{-2} + \varphi \cdot G_{R_i} \tag{6}$$

$$\varphi = Min(\varphi_{Isc}, \varphi_{Pmax}) \tag{7}$$

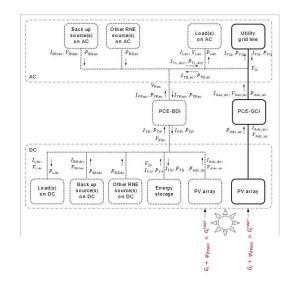
$$G_{E_i}[=]$$
 Equivalent Irradiance $\varphi[=]$ Bifaciality Coeff

PV Devices, Part 1-2 Measurement of I-V characteristics of Bifacial PV Devices



PV System performance, Part 1 - Monitoring





- Project Team formed and tasked with defining Bifacial PV performance standard following TC82 Plenary Meeting in Busan, S. Korea (Oct. 2019)
- Final draft edits to IEC 61724-1 complete. Project team is seeking comments by no later than 10/31/2019
- Major overhaul to defined terms were necessary (rear-side plane-ofarray irradiance, spectrally-corrected albedo, etc)
- Expect to have IEC 61724-1 revision with bifacial system consideration committee draft (CD) submitted within the 2019 calendar year

$$PR_{annual -eq,bi}^{i} = \left(\sum_{k} P_{out,k} \times \tau_{k}\right) / \left(\sum_{k} \frac{C_{k} \times P_{0} \times G_{i,k} \times BIF \times \tau_{k}}{G_{i,ref}}\right)$$

IEC bifacial standards development | IEC TC 82



IEC 61724-1 (WG3, TC82)

PV System performance, Part 1 - Monitoring



3.10

bifacial PV device

in a bifacial PV device, both surfaces (front and back sides) of the PV module are used for power generation.

3.11

bifaciality

bifaciality refers to the ratios between the main I-V characteristics of the back side and the front side of a bifacial device, typically at Standard Test Conditions (STC) unless otherwise specified. It is quantified with reference to bifaciality coefficients, namely the short-circuit current bifaciality coefficient φ_{lsc} , the open-circuit voltage bifaciality coefficient φ_{lsc} and the maximum power bifaciality coefficient $\varphi_{\text{\tiny Power}}$.

in-plane rearside irradiance ratio

the ratio of the irradiance incident on the rear side of the modules in the PV array to the irradiance incident on the front side of an inclined surface parallel to the plane of array. It is a dimensionless quantity but can exceed a value of 1 since, in addition to reflected light, diffuse

spectrally-corrected in-plane rearside irradiance ratio

 ρ_i^{SP}

the in-plane rearside irradiance ratio per 3.16 when both irradiance quantities are measured with a spectrally matched reference device or with the application of spectral correction factors per IEC 60904-7

3.17

spectrally matched reference device

a reference device (such as a PV cell or module) with spectral response characteristics sufficiently close to those of the PV modules in the PV array such that spectral errors are acceptably small under the typical range of incident spectra

in-plane rearside irradiance

Grear or POArear

is the sum of direct, diffuse, and ground-reflected irradiance incident on the rear side of the modules in the PV array, also known as rearside plane-of-array (POA^{rear}) irradiance.

Note 1 to entry: Expressed in units of W:m⁻².

Note 2 to entry (if measured via in-plane rearside irradiance ratio): $G_i^{rear} = \rho_i \times G_i$ OR $G_{i,SP}^{rear} = \rho_i^{SP} \times G_i$



Parameter	Symbol	Units	Monitoring purpose	Class A system		Class B system	
				Required?	Minimum number of sensors	Required?	Minimum numb
			Irradiance	(see section 8)			
Global horizontal irradiance	GHI	W⋅m ⁻²	Solar resource, connection to historical and satellite data	٧	1 × Table 3	√ or E	3.19 bifacial i
in-plane irradiance (POA)	$G_{\mathfrak{p}}$	W⋅m ⁻²	Solar resource	√	1 × Table 3	√	BIF
Horizontal albedo	РΗ	Unitless	Solar resource, rearside	√ Option 1 for bifacial	1 × Table 3		is a dime (G _i) to ca side colle
In-plane rearside irradiance (POA)	G _i rear	W⋅m ⁻²	Solar resource, rearside	√ Option 2 for bifacial	3 × Table 3		
Spectrally-corrected in- plane rearside irradiance	G ^{rear}	W⋅m ⁻²	Solar resource, rearside	Optional, for bifacial			
Direct normal irradiance	DNI	W⋅m ⁻²		√ for CPV	1 × Table 3		Note 2 to e
Diffuse irradiance	G_{d}	W⋅m ⁻²	Solar resource, concentrator	√ for CPV with < 20× concentration	1 × Table 3		same type

3.19

bifacial irradiance factor

is a dimensionless variable that can be directly multiplied by the frontside in-plane irradiance $(G_{
m i})$ to calculate the "effective" irradiance reaching a bifacial device from both the front and rear side collectively.

Note 1 to entry: $BIF = (1 + \varphi_{Pmax} \times \rho_i)$ OR $BIF^{sp} = (1 + \varphi_{Pmax} \times \rho_i^{SP})$

Note 2 to entry: rearside POA irradiance can be measured simultaneously with frontside POA irradiance using a bifacial reference cell. In that case, $BIF = G_i^{BIFi\,Ref\,Cell} \div G_i$ provided that frontside POA irradiance is measured with same type of device as the bifacial reference cell for consistency of the BIF calculation.





BIFACIAL PERFORMANCE MODELS AND PARAMETRIC SENSITIVITIES



Commercial Bifacial PV simulation software

Modeling assumptions in currently released versions





System Advisor Model 201

Incident irradiance on the gr Beam ground factor Fi	PVSyst	Features	NREL VF	
Diffuse ground factor 0 Shed transparent fraction 1	√	2D simulation of sheds	√	
Ground albedo 2 Reflected irradiance on back	√	Monthly albedo values	√	
Reemission form factor 2 Structure shading factor 11 PV array behavior	X	Circumsolar anisotropy for back side diffuse	X	ight 1 m
Mismatch loss factor 11 Module bifaciality factor 7	×	IAM for backside reflections	X	
4		Diffuse shading w/trackers		
		Irradiance non-uniformity		
		Spectral-corrected backside irradiance	.	
	*	Specular reflections	^	on
-2 -1 0 1 2 3 4 5 6 7 Dist	8 9 10 11 12 13 14 15 16 17 18 19 2 ance at ground level [m]	0 21 22	Divide row-to-row into n (100) seg Identify whether each segment is:	ments

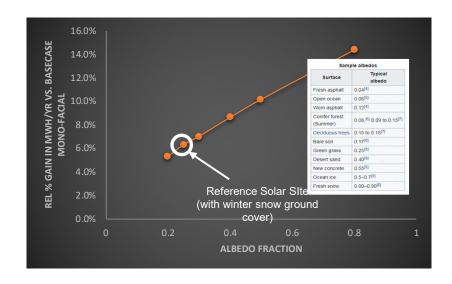
Commercially available PV sim software | Modeling Assumptions

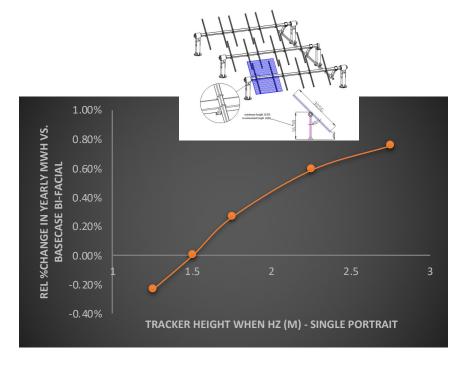
- IMEC, EnergyVille, PVCase releasing performance simulation model in 1H 2020
- PVLighthouse develops bifacial simulation using raytracing software with SPICE electrical PV model (Mismatch loss in bifacial modules due to non-uniform illumination in 1D tracking systems. McIntosh, K.R., Abbott, M.D., Sudbury, B.A., Meydbrey, J., 46th IEEE PVSC 2019)



Parametric sensitivities

Albedo, racking height (tracker)







Albedo | Racking height



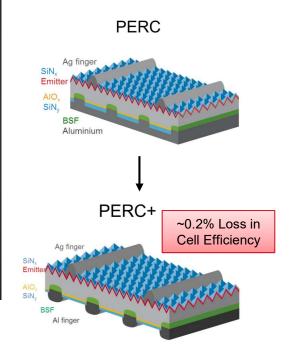
Parametric sensitivities

Bifaciality Factor

3.00% Heterojunction (HIT/HJT) 2.50% %CHANGE IN MWH/YR VS Limit of TOPcon/PERT 2.00% **BASECASE BI-FACIAL** Limit of p-1.50% type PERC+ 1.00% 0.50% 0.00% REL 65% 60% 70% 75% 80% 85% 90% 95% 100% -0.50% -1.00% **BIFACIALITY FACTOR**

PERC's bifacial capability is perhaps the key feature that will make the technology spread wider and reign longer than many anticipate...

- Shravan K. Chunduri, Michael Schmela "PERC solar cell technology 2018", Taiyang News.



T. Dullweber et al., 31st EUPVSEC (2015), p. 341
T. Dullweber et al., Prog. Photovolt.: Res. Appl., **24** (2016), p. 1487

PVSYST

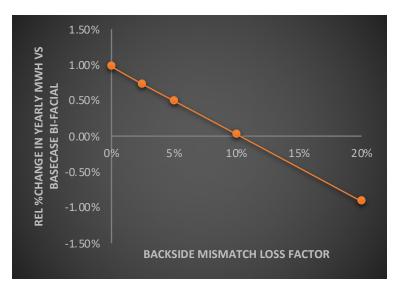
Parametric sensitivity | Bifaciality Factor

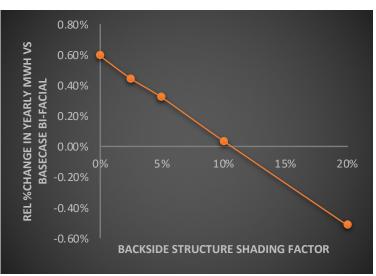
Every 1% increase in Annual Energy Production ~1.5¢/Wp in NPV



Parametric sensitivities

Structure shading, backside mismatch loss





- Initial Estimates (not based on field data):
 - 1. 2P Tracker = 5% Mismatch/2.5% Structure Shading
 - 2. 1P Tracker = 10% Mismatch/10% Structure Shading



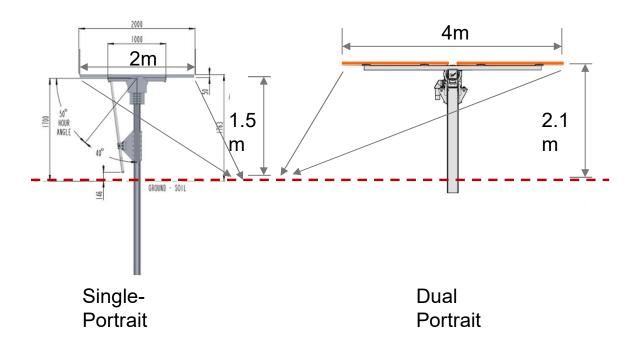
TOTAL IMPACT OF SHADING/MISMATCH ~1.5% on MWh/yr per 10% increase

Parametric Sensitivity | Structure shading / backside mismatch



Racking type (Tracker)

1P vs. 2P (single portrait/dual portrait)



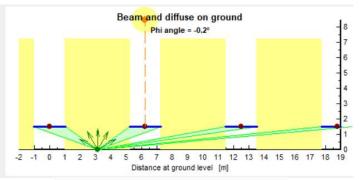
- Lower Aspect Ratio of Module Width to Tracker height produces better "ViewFactor"
- Single Portrait vs. Dual Portrait = 2% Gain in performance (fixing all other variables)

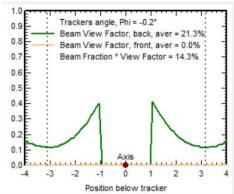




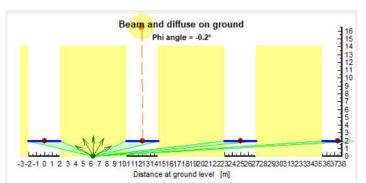
Racking type (Tracker) – Horizontal (noon)

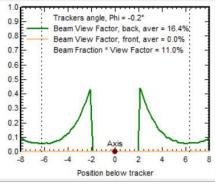
1P vs. 2P (single portrait/dual portrait)











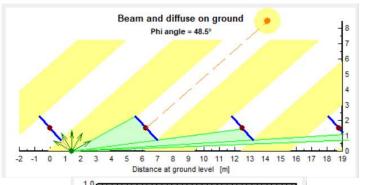
Dual Portrait

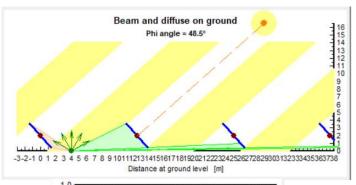




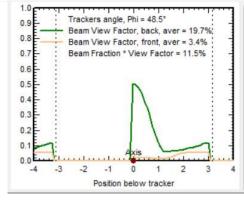
Racking type (Tracker) – Angled, morning/evening

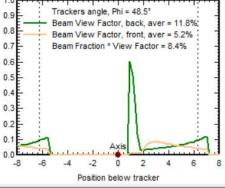
1P vs. 2P (single portrait/dual portrait)











Dual

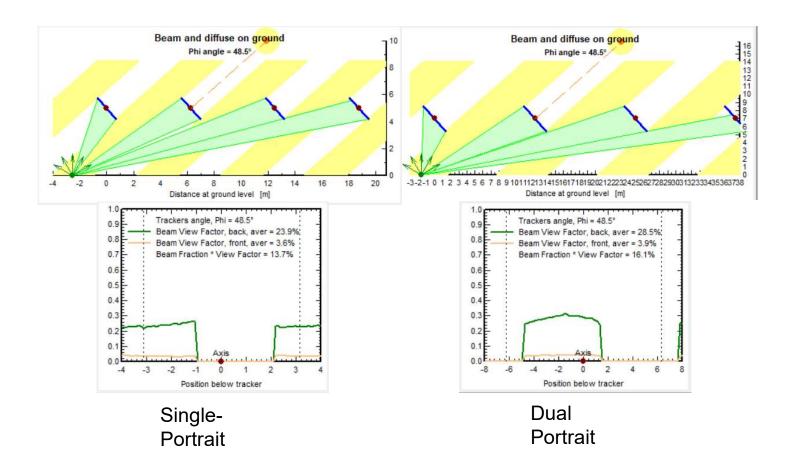
Portrait

PVSYST

Single-Portrait



Racking type (Tracker) — Unconstrained Height 1P vs. 2P (single portrait/dual portrait)









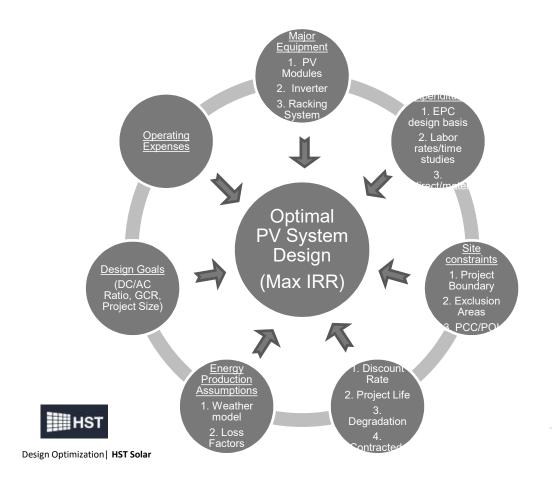
PROJECT ECONOMICS AND OPTIMIZATION OF SYSTEM DESIGN

Bifacial – The disruptive technology of our time



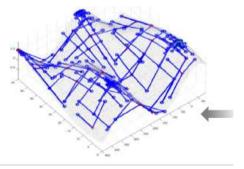
PV Plant Optimization Software

Multivariable optimization of design based on financial output





- ☐ Potential for 1000's of combinations
- □ All possible designs must be constrained by project boundaries & various exclusion areas
- Manual approach to design optimization is inherently limited...

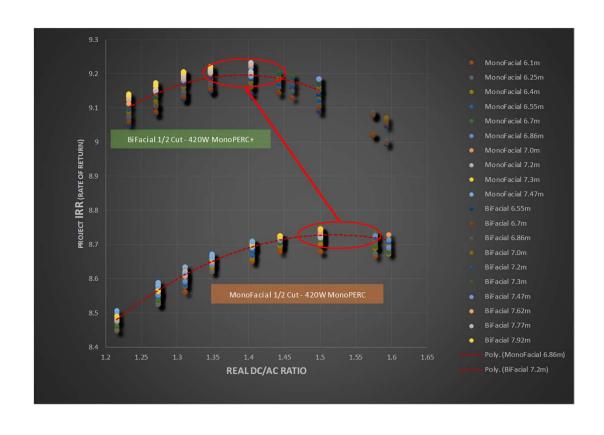




BIFACIAL VS. MONOFACIAL SYSTEM DESIGN OPTIMIZATIONS

Project site in Georgia (higher DHI/GHI)



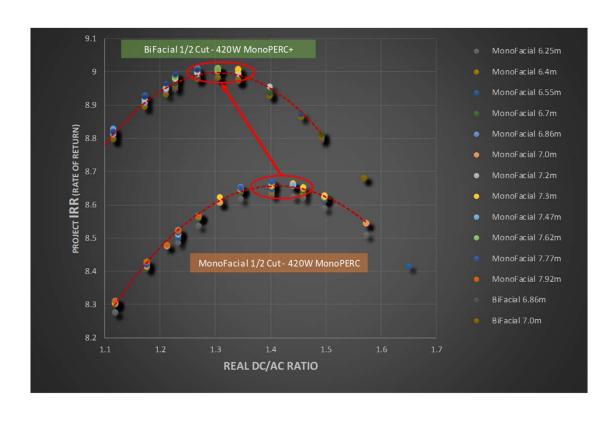




BIFACIAL VS. MONOFACIAL SYSTEM DESIGN OPTIMIZATIONS



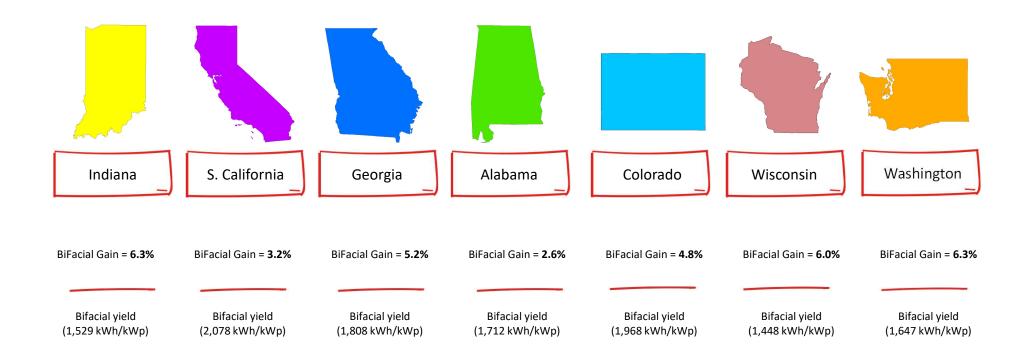






Modeled Bifacial gains around the U.S.

All horizontal SAT systems (relative gains, same GCR+DC/AC ratio)



Bifacial gains | Across the US



Summary and Conclusions



Bifacial adoption is happening much faster than anticipated



Performance guarantees will be challenging, but international standards will be necessary to pave the way



Modeling energy production of bifacial systems is in very early stages, but likely on the conservative side



Project economics are overwhelmingly favorable, but design and optimization require new ways of thinking







THANK YOU FOR YOUR ATTENTION

